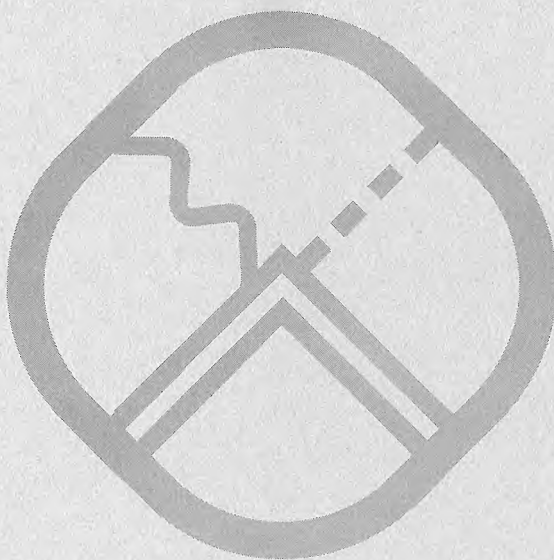


**EFFECTS OF MAGNET NON-LINEARITIES  
ON BETATRON OSCILLATION FREQUENCIES  
FOR THE 300 BEV PROTON SYNCHROTRON**

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APRIL 3, 1961



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## I. Introduction

The purpose of this note is to study the effects on betatron frequencies -- in particular, their variation with particle energy -- due to non-linear magnet fields. The idea is to determine whether non-linearities can be introduced deliberately in such a way that  $\nu$ , the number of betatron wavelengths in the circumference, is independent of particle energy for energies near the equilibrium energy. The result is that non-linearities of a magnitude such that the field index  $n$  varies by about 1 per cent per cm will suffice.

## II. Equations of Motion

The differential equations describing horizontal and vertical betatron oscillations are

$$\frac{d^2x}{ds^2} + \left[ k^2 \left( \frac{p_0}{p} - 1 \right) + \frac{e}{p} \frac{dB}{dx} \right] x = -k \left( \frac{p_0}{p} - 1 \right) - \left( k^3 \frac{p_0}{p} + 2k \frac{e}{p} \frac{dB}{dx} + \frac{e}{2p} \frac{d^2B}{dx^2} \right) x^2 + \dots \quad (1)$$

$$\frac{d^2z}{ds^2} - \frac{e}{p} \frac{dB}{dx} z = \left( 2k \frac{e}{p} \frac{dB}{dx} + \frac{e}{p} \frac{d^2B}{dx^2} \right) xz + \dots \quad (2)$$

respectively.  $s$  measures distance along the equilibrium orbit, in a counter-clockwise direction when viewed from above.  $x$  and  $z$  are the departures from the equilibrium orbit, outward and downward, respectively. The magnetic field in the orbit plane is assumed to be

$$B(x) = B + x \frac{dB}{dx} + \frac{1}{2} x^2 \frac{d^2B}{dx^2} + \dots$$

in a downward (+  $z$ ) direction. Note that  $B$ ,  $dB/dx$  and  $d^2B/dx^2$  are constants, measured at  $x = 0$ .  $k$  denotes the curvature of the equilibrium

orbit, traversed by a particle of momentum  $p_0$ ;  $p$  denotes the actual particle momentum. Balancing magnetic and centrifugal forces gives

$$B = \frac{p_0 k}{e} \quad (3)$$

We shall now summarize briefly the linear theory of oscillations about the equilibrium orbit<sup>1)</sup>; we set  $p = p_0$  and drop the non-linear terms on the right of Eqs. (1) and (2). Both equations are then of the form

$$\frac{d^2 y}{ds^2} + K(s) y = 0 \quad (4)$$

In an alternating-gradient synchrotron  $K(s)$  will be periodic with some period  $L$ , which may be the circumference  $C$  or some fraction of  $C$ . The general solution of (4) may be written

$$y(s) = A w(s) \cos [\psi(s) + \delta] \quad (5)$$

where  $A$  and  $\delta$  are arbitrary constants,  $w(s + L) = w(s)$ ,  $\psi(s + L) = \psi(s) + \mu$  and

$$\frac{d\psi}{ds} = \frac{1}{w^2} \quad (6)$$

$\mu$  is the betatron phase shift in  $L$ . The quantity  $w^2(s)$  is generally called  $\beta(s)$ ; according to Eq. (6), it represents the local betatron (reduced) wavelength.

The number of betatron oscillations in the machine circumference is

$$\nu = \frac{N\mu}{2\pi} \quad (7)$$

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1) A good review of the theory is given by Courant and Snyder, *Annals of Physics* 3, 1 (1958).

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where  $N$  is the number of identical sections;  $C = NL$ .

Now consider a small perturbation  $\delta(s)$  in  $K(s)$ ; that is, consider instead of Eq. (4) the equation

$$\frac{d^2 y}{ds^2} + [K(s) + \delta(s)] y = 0 \quad (8)$$

It can be shown<sup>1,2)</sup> that, to first order in  $\delta$ , the change in  $\nu$  is given by

$$\Delta\nu = \frac{1}{4\pi} \oint \delta(s) \beta(s) ds$$

where  $\oint$  denotes an integral around the entire machine circumference.

### III Effects of Synchrotron Oscillations

Suppose now that the particle momentum  $p$  differs slightly from the equilibrium momentum  $p_0$ . The equilibrium orbit is then shifted outward by an amount  $X(s)$ . We now write

$$x(s) = X(s) + \xi(s) \quad (9)$$

where  $\xi$  describes the rapid horizontal betatron oscillations about the slowly varying orbit  $X$ . Substituting Eq. (9) into (1) and (2), we obtain the differential equations

$$\begin{aligned} \frac{d^2 \xi}{ds^2} + \left[ k^2 \left( 1 - 2 \frac{\Delta p}{p_0} \right) + \frac{e}{p} \frac{dB}{dx} + 2X \left( k^3 \frac{p_0}{p} + 2k \frac{e}{p} \frac{dB}{dx} \right. \right. \\ \left. \left. + \frac{e}{2p} \frac{d^2 B}{dx^2} \right) \right] \xi = 0 \end{aligned} \quad (10)$$

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2) L. S. Smith, Internal Report IS-4, Brookhaven National Laboratory.

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$$\frac{d^2 z}{ds^2} + \left[ -\frac{e}{p} \frac{dB}{dx} - X \left( 2k \frac{e}{p} \frac{dB}{dx} + \frac{e}{p} \frac{d^2 B}{dx^2} \right) \right] z = 0 \quad (11)$$

where we have linearized in the small quantities  $\xi$  and  $z$ .

Equations (10) and (11) are now of the form (8). The unperturbed  $K(s)$  for  $p = p_0$  are

$$K = \begin{cases} k^2 + \frac{e}{p_0} \frac{dB}{dx} & \text{(horizontal oscillations)} \\ -\frac{e}{p_0} \frac{dB}{dx} & \text{(vertical oscillations)} \end{cases}$$

so that the horizontal and vertical perturbations  $\delta(s)$  are

$$\delta_h = -2k^2 \frac{\Delta p}{p_0} - \frac{\Delta p}{p_0} \frac{e}{p_0} \frac{dB}{dx} + 2X \left( k^3 + 2k \frac{e}{p_0} \frac{dB}{dx} + \frac{e}{2p_0} \frac{d^2 B}{dx^2} \right)$$

$$\delta_v = \frac{\Delta p}{p_0} \frac{e}{p_0} \frac{dB}{dx} - X \left( 2k \frac{e}{p_0} \frac{dB}{dx} + \frac{e}{p_0} \frac{d^2 B}{dx^2} \right)$$

It is conventional to define  $n = \frac{-1}{kB} \frac{dB}{dx} = -\frac{e}{p_0 k^2} \frac{dB}{dx}$ . This gives

$$\delta_h = \frac{\Delta p}{p_0} (n - 2)k^2 + 2X \left[ k^3(1 - 2n) + \frac{e}{2p_0} \frac{d^2 B}{dx^2} \right] \quad (12)$$

$$\delta_v = -n k^2 \frac{\Delta p}{p_0} - X \left( -2n k^3 + \frac{e}{p_0} \frac{d^2 B}{dx^2} \right) \quad (13)$$

Two simplifications can now be made. In the first place,  $|n| \gg 1$  (for the 300 Bev machine,  $|n| \sim 10^4$ ). In the second place, we can use



the large value of  $v$  ( $\sim 40$ ) as follows: Smith<sup>2)</sup> gives the approximation

$$X(s) \approx \frac{\Delta p}{p_0} \langle k \beta^{3/2} \rangle \beta^{1/2}(s) \quad (14)$$

where  $\langle \rangle$  denotes an average over  $s$  around the circumference. Therefore, omitting factors of order one,

$$X \sim \frac{\Delta p}{p_0} k \beta^2$$

From Eqs. (6) and (7),

$$\beta \sim \frac{c}{2\pi v} \frac{R}{v}$$

where  $R$  is the machine radius  $\frac{c}{2\pi}$ . Therefore

$$X \sim \frac{\Delta p}{p_0} \frac{kR^2}{v^2} \sim \frac{\Delta p}{p_0} \frac{R}{v^2} \sim \frac{\Delta p}{p_0} \frac{1}{kv^2} \quad (15)$$

The large value of  $v$ , coupled with (15), enables us to omit the  $X k^3$  terms in Eqs. (12) and (13). Thus, (12) and (13) become

$$\delta_h = n k^2 \frac{\Delta p}{p_0} + \frac{k}{B} \frac{d^2 B}{dx^2} X$$

$$\delta_v = -n k^2 \frac{\Delta p}{p_0} - \frac{k}{B} \frac{d^2 B}{dx^2} X$$

We made use of Eq. (3) to simplify the last term in each.

The change in effective gradient length with orbit position produces a significant shift in  $v$  for the Brookhaven AGS, and we shall therefore include this effect. According to Smith<sup>2)</sup>, this contributes to  $\begin{pmatrix} \delta_h \\ \delta_v \end{pmatrix}$  a term

$$\mp \frac{1}{2} |n| k^2 \left| \frac{dI_g}{dX} \right| X \delta(s)_{\text{end}}$$

where  $\delta(s)_{\text{end}}$  consists of a delta function at each end of every magnet.

We may summarize by observing that there are three perturbing terms in  $\delta_h$  (and  $\delta_v$ ), due to momentum error, magnet non-linearity, and variation in gradient length. Also, note that  $\delta_h = -\delta_v$  in this approximation.

#### IV Numerical Estimates

Since no definite magnet lattice has been arrived at for the 300 Bev machine, we have adopted some tentative and approximate numbers. We shall assume

$$R = 1300 \text{ m}$$

$$k = (1000 \text{ m})^{-1}$$

$$n = \pm 10^4$$

$$N = 30$$

$$\nu = 40$$

Each of the 30 "superperiods" contains 32 magnets, 16 radially focussing (F) and 16 radially defocussing (D). Each magnet is 7 meters long. The phase shift per unit length is

$$\frac{2\pi\nu}{C} = \frac{\nu}{R} \approx 3 \times 10^{-2} \text{ m}^{-1}$$

so that  $\beta \approx 33 \text{ m}$ . We shall assume that  $\beta$  oscillates between 20 m and 50 m; more precisely, we assume

$$\beta_h = \begin{cases} 20 \text{ m} & \text{in D magnets} & (n = + 10^4) \\ 50 \text{ m} & \text{in F magnets} & (n = - 10^4) \end{cases}$$

For vertical oscillations the situation is reversed;  $\beta_v = 20 \text{ m}$  in F magnets and  $50 \text{ m}$  in D magnets.

For  $X(s)$  we shall make the approximation (14). For our assumed lattice

$$\begin{aligned} \langle k \beta^{3/2} \rangle &\approx \frac{1}{1.3} \cdot \frac{1}{1000} \cdot \frac{20^{3/2} + 50^{3/2}}{2} \\ &\approx 0.17 \text{ m}^{1/2} \end{aligned}$$

Thus

$$X(s) \approx \begin{cases} 0.76 \frac{\Delta p}{p_0} \text{ m} & \text{in D magnets} \\ 1.20 \frac{\Delta p}{p_0} \text{ m} & \text{in F magnets} \end{cases}$$

We shall now separately estimate the three effects referred to in the previous section:

(a) Variation in gradient length -

$$\begin{aligned} \Delta v_h &= \frac{1}{4\pi} \oint \beta_h(s) \delta_h(s) ds \\ &= \frac{-1}{8\pi} |n| k^2 \left| \frac{dI_g}{d\bar{X}} \right| \sum_{\text{ends}} X(s) \beta_h(s) \end{aligned}$$

A reasonable estimate for  $\left| \frac{dI_g}{d\bar{X}} \right|$  seems to be 0.5. Also

$$\sum_{\text{ends}} X(s) \beta_h(s) \approx 960 \left[ (0.76) \times (20) + (1.20) \times (50) \right] \frac{\Delta p}{p_o}$$

$$\approx 7.2 \times 10^4 \frac{\Delta p}{p_o} m^2$$

Therefore

$$\Delta v_h \approx \frac{-1}{8\pi} \frac{10^4}{10^6} (0.5) (7.2 \times 10^4) \frac{\Delta p}{p_o}$$

$$\approx -14.3 \frac{\Delta p}{p_o}$$


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For vertical oscillations

$$\Delta v_v = \frac{+1}{8\pi} |n| k^2 \left| \frac{dI_g}{dX} \right| \sum_{\text{ends}} X(s) \beta_v(s)$$

Estimating as before

$$\sum_{\text{ends}} X(s) \beta_v(s) \approx 960 \left[ (0.76) \times (50) + (1.20) \times (20) \right] \frac{\Delta p}{p_o}$$

$$\approx 6.0 \times 10^4 \frac{\Delta p}{p_o} m^2$$

and

$$\Delta v_v \approx +11.9 \frac{\Delta p}{p_o}$$


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(b) Momentum error -

$$\Delta v_h = \frac{1}{4\pi} \frac{\Delta p}{p_o} \oint n k^2 \beta_h ds$$

$$\oint n k^2 \beta_h ds \approx \frac{10^4}{10^6} (480)(7)(20 - 50)$$

$$\approx - 1010$$

so that

$$\underline{\underline{\Delta v_h \approx - 80 \frac{\Delta p}{p_o}}}$$

A similar calculation gives

$$\underline{\underline{\Delta v_v \approx - 80 \frac{\Delta p}{p_o}}}$$

(c) Magnet non-linearity -

$$\Delta v_h = \frac{1}{4\pi} \oint \frac{k}{B} \frac{d^2 B}{dx^2} \times \beta_h ds$$

Let us assume

$$\frac{1}{k^2 B} \frac{d^2 B}{dx^2} = \begin{cases} A & \text{in D magnets} \\ B & \text{in F magnets} \end{cases}$$

Then

$$\Delta v_h \approx \frac{(480)(7)}{4\pi \times 10^9} \frac{\Delta p}{p_o} [(0.76)(20)A + (1.20)(50)B]$$

$$\underline{\underline{\Delta v_h \approx (4.1 a + 16.1 b) \frac{\Delta p}{p_o}}}$$

where we have set

$$a = 10^{-6} A, \quad b = 10^{-6} B$$

Similarly

$$\Delta v_v \approx - \frac{(480)(7)}{4\pi \times 10^9} \frac{\Delta p}{p_0} \left[ (0.76)(50)A + (1.20)(20)B \right]$$

$$\Delta v_v \approx (-10.2 a - 6.4 b) \frac{\Delta p}{p_0}$$


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#### V Optimum Amount of Non-linearity

Collecting the numerical results of the previous section, we have

$$\Delta v_h = (-14.3 - 80 + 4.1 a + 16.1 b) \frac{\Delta p}{p_0}$$

$$\Delta v_v = (11.9 - 80 - 10.2 a - 6.4 b) \frac{\Delta p}{p_0}$$

We have exhibited explicitly the variation in gradient length effect, the momentum error effect, and the magnet non-linearity effects, in that order. Note that here, in contrast to the Brookhaven AGS, the first effect is quite small compared to the second.

If we choose

$$a = 0.7 - 13.0 = -12.3$$

(16)

$$b = 0.7 + 8.3 = +9.0$$

the effects cancel and  $v_h$  and  $v_v$  are independent of  $\frac{\Delta p}{p_0}$ . In Eq. (16) the gradient length and momentum error contributions are presented separately, in that order.

Note that

$$\begin{aligned}\frac{\Delta n}{\Delta x} &= \frac{-1}{kB} \frac{d^2 B}{dx^2} \\ &= -kA \quad \text{or} \quad -kB \\ &= -10^3 a \quad \text{or} \quad -10^3 b\end{aligned}$$

Thus the result is that

$$n = \begin{cases} 10,000 + 123 x_{\text{cm}} & \text{in D magnets} \\ -10,000 - 90 x_{\text{cm}} & \text{in F magnets} \end{cases}$$

where  $x_{\text{cm}}$  is simply  $x$  expressed in centimeters.

These non-linearities are clearly achievable; the accuracy with which they can be maintained would appear to be a more serious problem.





